



Novella, D., Dolejš, D., Myhill, R., Pamato, M. G., Manthilake, G., & Frost, D. J. (2017). Melting phase relations in the systems  $\text{Mg}_2\text{SiO}_4\text{-H}_2\text{O}$  and  $\text{MgSiO}_3\text{-H}_2\text{O}$  and the formation of hydrous melts in the upper mantle. *Geochimica et Cosmochimica Acta*, 204, 68-82.  
<https://doi.org/10.1016/j.gca.2016.12.042>

Peer reviewed version

Link to published version (if available):  
[10.1016/j.gca.2016.12.042](https://doi.org/10.1016/j.gca.2016.12.042)

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**1 Melting phase relations in the systems  $\text{Mg}_2\text{SiO}_4\text{-H}_2\text{O}$  and  $\text{MgSiO}_3\text{-H}_2\text{O}$  and the**  
**2 formation of hydrous melts in the upper mantle**

3

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24 **Abstract**

25 High-pressure and high-temperature melting experiments were conducted in the systems  
26  $\text{Mg}_2\text{SiO}_4\text{-H}_2\text{O}$  and  $\text{MgSiO}_3\text{-H}_2\text{O}$  at 6 and 13 GPa and between 1150 to 1900 °C in order to  
27 investigate the effect of  $\text{H}_2\text{O}$  on melting relations of forsterite and enstatite. The liquidus  
28 curves in both binary systems were constrained and the experimental results were  
29 interpreted using a thermodynamic model based on the homogeneous melt speciation  
30 equilibrium,  $\text{H}_2\text{O} + \text{O}^{2-} = 2 \text{OH}^-$ , where water in the melt is present as both molecular  $\text{H}_2\text{O}$   
31 and  $\text{OH}^-$  groups bonded to silicate polyhedra. The liquidus depression as a function of  
32 melt  $\text{H}_2\text{O}$  concentration is predicted using a cryoscopic equation with the experimental  
33 data being reproduced by adjusting the water speciation equilibrium constant. Application  
34 of this model reveals that in hydrous  $\text{MgSiO}_3$  melts at 6 and 13 GPa and in hydrous  
35  $\text{Mg}_2\text{SiO}_4$  melts at 6 GPa, water mainly dissociates into  $\text{OH}^-$  groups in the melt structure.  
36 A temperature dependent equilibrium constant is necessary to reproduce the data,  
37 however, implying that molecular  $\text{H}_2\text{O}$  becomes more important in the melt with  
38 decreasing temperature. The data for hydrous forsterite melting at 13 GPa are  
39 inconclusive due to uncertainties in the anhydrous melting temperature at these  
40 conditions. When applied to results on natural peridotite melt systems at similar  
41 conditions, the same model infers the presence mainly of molecular  $\text{H}_2\text{O}$ , implying a  
42 significant difference in physiochemical behavior between simple and complex hydrous  
43 melt systems. As pressures increase along a typical adiabat towards the base of the upper  
44 mantle, both simple and complex melting results imply that a hydrous melt fraction  
45 would decrease, given a fixed mantle  $\text{H}_2\text{O}$  content. Consequently, the effect of pressure

on the depression of melting due to H<sub>2</sub>O could not cause an increase in the proportion, and hence seismic visibility, of melts towards the base of the upper mantle.

**Keywords:** olivine, enstatite, phase equilibria, hydrous melting, cryoscopic equation, water speciation.

## 1. Introduction

The effect of H<sub>2</sub>O on the formation of silicate melts underlies a number of igneous processes taking place within the Earth's mantle. H<sub>2</sub>O has an important influence on the generation of magmas at subduction zones being both a metasomatic agent of the arc magma source region and responsible for the high degrees of melting that produce these magmas (e.g. Tatsumi et al., 1986). The lithospheric mantle shows abundant evidence for metasomatism by H<sub>2</sub>O-bearing melts (e.g. Menzies and Hawkesworth, 1987; Erlank et al. 1987) and several exotic magma types such as kimberlites and lamproites are likely formed, at least in part, as a result of H<sub>2</sub>O lowering the mantle solidus (e.g. Kushiro et al., 1968; Kawamoto and Holloway, 1997; Sokol et al., 2013). H<sub>2</sub>O induced melting of the deep mantle has also been proposed to explain a number of geophysical observations such as the Earth's seismic low velocity zone (Lambert and Wyllie, 1970; Mierdel et al., 2007) and possible low velocity layers present on top of the transition zone (Tauzin et al., 2010) and immediately below it (Schmandt et al., 2014). Recently, it was proposed that H<sub>2</sub>O-induced melts would tend to migrate in the lower mantle, and transfer H<sub>2</sub>O from ultramafic to mafic lithologies, as a result of the difference in H<sub>2</sub>O storage capacities of these rock types (Pamato et al., 2015).

69

70 In order to understand the production of hydrous melts in the Earth's mantle it is  
71 important to constrain how H<sub>2</sub>O affects the melting behaviour of mantle materials. In this  
72 regard, a number of studies have been performed to quantify the effects of H<sub>2</sub>O on  
73 lowering melting temperatures and increasing melt yields in natural mantle rock systems  
74 (Mysen and Boettcher, 1975; Hirose and Kawamoto, 1995; Gaetani and Grove, 1998;  
75 Balta et al., 2011; Tenner et al., 2012b; Novella et al., 2014). Determining the effect of  
76 H<sub>2</sub>O on melting in natural chemical systems is challenging, however, due to the large  
77 number of chemical components that are potentially influenced by H<sub>2</sub>O. These  
78 determinations are further complicated by a number of other instrumental factors, such as  
79 control of oxygen fugacity, attainment of equilibrium, H<sub>2</sub>O and FeO loss from  
80 experimental capsules and the difficulty in determining the H<sub>2</sub>O contents of melts  
81 (Brooker et al., 1998; Liu et al., 2006; Tenner et al., 2012b; Novella and Frost, 2014).

82

83 It has long been appreciated that the effects of H<sub>2</sub>O on silicate melts can be more easily  
84 quantified by examining melting behavior in simple systems (Kushiro et al, 1968;  
85 Kushiro and Yoder, 1969; Kushiro, 1972; Hodges, 1973, 1974). From results of  
86 experiments in simple systems such as Mg<sub>2</sub>SiO<sub>4</sub>-SiO<sub>2</sub>-H<sub>2</sub>O, Kushiro (1972) proposed, for  
87 example, that hydrous mantle partial melts would be more SiO<sub>2</sub>-rich compared to dry  
88 melts. Studies in simple systems can also be used to quantify the effect of H<sub>2</sub>O on mineral  
89 melting at high pressures and experiments have been performed up to conditions  
90 equivalent to those in the mantle transition zone (Kushiro and Yoder, 1969; Luth, 1993;  
91 Inoue, 1994). While relatively detailed melting phase relations on hydrous forsterite

(Kushiro and Yoder, 1969; Hodges 1973) and enstatite (Kushiro and Yoder, 1969; Kushiro et al., 1968) exist up to 3 GPa, phase relations at higher pressures are more sparse and show less mutual agreement. Luth (1993) and Inoue (1994) investigated the melting behavior of forsterite with 17-20 wt% H<sub>2</sub>O up to pressures of 12 and 15.5 GPa, respectively, although the two studies are in poor agreement. In addition, Inoue (1994) also studied the phase relations of hydrous enstatite and an intermediate Mg/Si ratio composition to similar pressures. However, in this previous study more emphasis was placed on determining the conditions of the hydrous solidus rather than quantifying the effect of melt H<sub>2</sub>O content on the melting temperature.

Recently, several studies on natural multicomponent systems have proposed generalized models for the effects of H<sub>2</sub>O on peridotite melting temperatures (Medard and Grove, 2008; Tenner et al., 2012a). While such models are quite successful in reproducing the experimental observations, they make assumptions concerning both the thermodynamic data and the mechanism by which H<sub>2</sub>O dissolves in melts that can be more easily tested using results on simplified systems. In simplified systems additional constraints are also provided by calorimetric measurements such as those performed to determine the entropy of melting (Bottinga, 1985; Navrotsky et al., 1989; Richet et al., 1993; Tangeman et al., 2001). One advantage of examining experiments in simple systems is that treatment with relatively simple thermodynamic models should provide a firmer basis for understanding hydrous melting on a physicochemical level (Burnham, 1975; Silver and Stolper, 1985) and can be used to examine how the effect of H<sub>2</sub>O on melting may be further modified by pressure.

115

116 The goal of this study is to determine the melting phase relations in the systems  $\text{Mg}_2\text{SiO}_4$ -  
117  $\text{H}_2\text{O}$  and  $\text{MgSiO}_3$ - $\text{H}_2\text{O}$  at upper mantle conditions. In particular, we investigate the  $\text{H}_2\text{O}$   
118 contents of melts in equilibrium with forsterite and/or enstatite as a function of  
119 temperature at high pressure by bracketing the location of the hydrous liquidus curves.  
120 The experimental data are analysed using thermodynamic models to provide insight into  
121 the  $\text{H}_2\text{O}$  dissolution mechanism and its effects at high pressures. Results are presented for  
122 both systems at 6 and 13 GPa corresponding to  $\sim 180$  and  $\sim 390$  km depth in the mantle,  
123 and temperatures ranging between 1150 to 1900 °C.

124

## 125 **2. Experimental and analytical details**

126 Two sets of compositions were prepared for experiments in the systems  $\text{Mg}_2\text{SiO}_4$ - $\text{H}_2\text{O}$   
127 and  $\text{MgSiO}_3$ - $\text{H}_2\text{O}$ . In the system  $\text{Mg}_2\text{SiO}_4$ - $\text{H}_2\text{O}$ , starting compositions were mixed from  
128 two end-member compositions:  $\text{Mg}_2\text{SiO}_4$  (forsterite) synthesized from high purity oxides,  
129  $\text{MgO}$  and  $\text{SiO}_2$ , and a 2:1 molar mixture of  $\text{Mg}(\text{OH})_2$  (brucite) and  $\text{SiO}_2$ . The pure  
130 forsterite was synthesized by firing the oxides at 1500 °C for 2 hours and then grinding  
131 the sintered mix for 1 hour under ethanol. This firing and grinding process was repeated 4  
132 times. The 2:1 brucite-silica mixture corresponds to a composition of  $\text{Mg}_2\text{SiO}_4$  with 20.4  
133 wt%  $\text{H}_2\text{O}$  in the bulk. In order to prepare this end member, brucite and  $\text{SiO}_2$  were dried  
134 overnight at 120 °C and 1000 °C, respectively. The calculated amount of each component  
135 was then weighed, ground for 1 hour under ethanol and dried under an infrared lamp. By  
136 varying the mass proportions of the end member compositions a range of mixtures were  
137 prepared with variable  $\text{H}_2\text{O}$  content but with a constant stoichiometry of  $\text{Mg}/\text{Si} = 2$  (Table

1). All mixtures with water contents less than 20.4 wt% were prepared by grinding the weighed proportions of dry forsterite and forsterite with 20.4 wt% bulk H<sub>2</sub>O for 30 minutes under ethanol, and then drying. Before each mixture was prepared the forsterite end-member was dried at 1000 °C for one hour and the water-bearing forsterite end-member was dried overnight at 120 °C. This approach was also followed for the preparation of starting mixtures in the system MgSiO<sub>3</sub>-H<sub>2</sub>O. In this case, an end-member 1:1 molar mixture of brucite and SiO<sub>2</sub>, corresponding to a composition of MgSiO<sub>3</sub> with 15.2 wt% bulk H<sub>2</sub>O, was initially prepared (Table 1). The dry end-member MgSiO<sub>3</sub> was prepared from high purity oxides MgO and SiO<sub>2</sub> and the dry and hydrous end-members were mixed in different mass proportions to obtain the compositions given in Table 1. Once prepared, all final mixtures were stored in a furnace at 120 °C to limit the adsorption of water.



150

151 Platinum or platinum/rhodium multi-chamber capsules were fabricated from 2 mm  
152 diameter Pt or Pt/Rh (Pt<sub>90</sub>Rh<sub>10</sub>) rods cut into 1 mm long sections. The resulting discs were  
153 spark eroded on one surface, obtaining rows of 4 to 6 chambers per disc with the  
154 chambers being 0.25 mm in diameter and approximately 0.66 mm deep. Each chamber  
155 was loaded with a different starting powder such that H<sub>2</sub>O contents increased across the  
156 row of chambers. Sample powders were packed into each chamber using a tungsten-  
157 rhenium needle. When packed sufficiently the chambers remained full even when air was  
158 blown over the surface. Blowing air removed extraneous sample powders from chambers  
159 that had not yet been loaded. The Pt capsules were closed by placing a second Pt disc  
160 0.25 mm thick on top of the chambers, which was held closed under pressure. When  
161 Pt/Rh capsules were employed the open extremities of the chambers were closed by  
162 placing on top 6 foils of Pt/Rh with total thickness of ~0.25 mm.

163

164 High pressure and high temperature experiments were carried out using a multianvil  
165 apparatus installed at the Bayerisches Geoinstitut (BGI). The experiments were  
166 performed in an 18/11 assembly, with an 18 mm edge length Cr<sub>2</sub>O<sub>3</sub>-doped MgO  
167 octahedral pressure medium and 11 mm WC-anvil corner truncations. Experiments at 6  
168 GPa were performed using a 500 tonne Walker-type multi anvil press and a 5000 tonne  
169 Kawai-type multianvil press. The experiments at 13 GPa were carried out only with the  
170 5000 tonne multianvil apparatus. The pressure calibration at 6 GPa was performed using  
171 the CaGeO<sub>3</sub> garnet to perovskite phase transition (Ross et al, 1986) for the 500 tonne  
172 multianvil apparatus, while the pressure calibration described by Frost et al. (2004) was

employed for the experiments performed with the 5000 tonne press. A stepped graphite heater was used in the experiments at 6 GPa, while for those performed at 13 GPa a stepped  $\text{LaCrO}_3$  heater was employed. Temperatures during the experiments were monitored using a  $\text{W}_{97}\text{Re}_3\text{--W}_{75}\text{Re}_{25}$  (D type) thermocouple inserted within an alumina sleeve. The thermocouple junction was in contact with the base of the spark eroded capsules,  $\sim 0.5$  mm from the sample chambers, with an estimated temperature uncertainty of  $50^\circ\text{C}$  (Frost et al., 2004). However, higher uncertainty ( $100^\circ\text{C}$ ) is considered for experiments where the thermocouple reading failed and temperature was determined based on power-temperature calibrations. A  $25\text{ }\mu\text{m}$  thick foil of rhenium was placed on the top of the capsule in order to avoid direct contact between the capsule and the thermocouple junction. The maximum temperature fluctuation during the experiments was  $\pm 5^\circ\text{C}$ . The capsule was surrounded by MgO spacers and sleeves. Each experiment was first pressurised over 4 hours then heated in  $\sim 15$  minutes to target temperature where it remained for up to 30 minutes depending on target temperature. Once completed, the experiment was quenched by turning off the power supply to the graphite/ $\text{LaCrO}_3$  heater, and decompression was carried out over approximately 15 hours.

After each experiment, the Pt or Pt/Rh sample disk was recovered, mounted in epoxy and polished in the absence of water. Due to the high porosity of the charges, impregnation with either epoxy resin or superglue was often required in order to avoid loss of material during the polishing. Once the samples were polished, phase identification and chemical analyses were carried out using a JEOL-JXA-8200 electron microprobe (EMPA) at the BGI. Conditions of 15 kV and 15 nA for the accelerating voltage and beam current,

respectively, were adopted in all the analyses, using a beam diameter of  $\sim 1\ \mu\text{m}$ . Standards for  $\text{SiO}_2$  and  $\text{MgO}$  were forsterite and enstatite, respectively, and all the analyses were processed following the ZAF corrections.

Raman spectroscopy was conducted on some of the experimental charges to confirm the nature of the mineral phases produced. The analyses were performed using a LABRAM Raman spectrometer installed at the BGI and operating with a He-Ne laser with 632 nm red-line wavelength. Analyses were performed with a total of 3 spectrum collections and an accumulation time of 15 seconds each.

### **3. Results**

Sections of typical experimental runs are shown in Fig. 1. At both pressures of 6 and 13 GPa melts quenched to produce a fine intergrowth of crystals. However, crystals that were solid phases during heating of the experiments were easily distinguished from the quenched crystals based on their euhedral character and grain size. In some experiments quenched areas with different grain sizes and crystallite shapes could be observed that might be interpreted as separate coexisting liquids, or vapour (Fig. 1a). Given that the  $\text{H}_2\text{O}$  contents of the charges are relatively low for fluid-saturated conditions to be encountered (e.g. Mibe et al., 2002), it seems more likely that these differences in texture result from local differences in nucleation and growth during quenching of the experiments. All quench textures are consistent with an origin as  $\text{H}_2\text{O}$ -bearing melts rather than aqueous fluids. This distinction is made based on the quench crystal density

compared to previous studies performed at lower temperatures where a sub-solidus aqueous fluid phase was encountered (Mibe et al. 2002).

Sections were ground by hand to over half way through the sample chambers to verify the absence of crystals in experiments interpreted to have encountered superliquidus conditions. Continual checks were made during grinding to examine for crystals that might not otherwise appear in the final section. Some samples were ground more than 80% through to ensure that no crystals were present in the charge. The small size of the sample chambers should ensure that thermal gradients across the samples are minimal. The large relative size of the metal capsule should also help to relax thermal gradients. Based on measurements performed in similar assemblies using two pyroxene thermometry (Brey et al., 1990), the thermal gradients within each chamber are estimated to be  $<20^{\circ}\text{C}$ .

Several experiments were performed at the same conditions but with different heating durations in order to assess  $\text{H}_2\text{O}$  loss from the Pt capsules during the experiments. Two experiments loaded with the same starting mixtures were performed at 6 GPa and  $1400^{\circ}\text{C}$  for 5 and 30 minutes, respectively, and in both cases the resulting assemblages in each of the sample chambers were identical. At 13 GPa the same result was obtained in two experiments performed at  $1450^{\circ}\text{C}$ . These observations imply that significant loss of  $\text{H}_2\text{O}$  does not occur in experiments with run durations up to 30 minutes at temperatures up to  $1450^{\circ}\text{C}$ . However, it was observed that in some experiments performed at higher temperatures ( $>1650^{\circ}\text{C}$ ), run durations greater than 30 minutes led to substantial

crystallisation, likely due to H<sub>2</sub>O loss from the Pt capsule. Therefore, experiments performed above 1650 °C were held at target temperature for 5-20 minutes only.

### **3.1 Experimental results at 6 GPa**

Experimental conditions and phase assemblages of the runs performed at 6 GPa for both Mg<sub>2</sub>SiO<sub>4</sub>-H<sub>2</sub>O and MgSiO<sub>3</sub>-H<sub>2</sub>O systems are summarized in Table 2. In the forsterite-H<sub>2</sub>O system, experiments were performed from 1250 to 1650 °C (Fig. 2). In some runs performed at 1250 °C crystals of enstatite were also observed, possibly suggesting incongruent melting at these conditions. However, this observation is not in agreement with the experimental results of Inoue (1994), which indicate the transition from congruent to incongruent melting of forsterite in the system Mg<sub>2</sub>SiO<sub>4</sub>-H<sub>2</sub>O to occur between 7.7 and 12 GPa. Rather than incongruent melting, the appearance of enstatite is possibly due to slight variations of certain starting mixtures from the Fo-H<sub>2</sub>O join, which would be more visible at high degrees of crystallization. Our data suggest that the invariant curve Fo + En = Liquid is passing very close to the fo-H<sub>2</sub>O line and possibly crossing it (Fig. 3), explaining the observed phase relations (Table 2). In experiments conducted at temperatures above 1250 °C, the run products contained either forsterite and melt or melt only, implying congruent melting. The run with the highest H<sub>2</sub>O content (20.4 wt%) produced crystals in equilibrium with quenched melt at 1250 °C, hence it had not yet reached the liquidus temperature (Table 2). However, at temperatures higher than 1250 °C, most experiments had one or more chambers that contained a supraliquidus product that comprised only quenched melt. At 1400 °C, for example, forsterite crystals coexisting with melt were produced in charges with H<sub>2</sub>O contents of 7.9, 9.7, 13.8 wt%,

but the run with 18.3 wt% H<sub>2</sub>O contained only hydrous melt (Fig. 1b, Table 2). The proportion of crystals in each of these runs decreases in agreement with the lever rule as the crystal-melt region is crossed as a function of H<sub>2</sub>O content in the system. No interpretation of these proportions is made, however, as it may be inaccurate due to the particular sample section obtained during polishing.

In the MgSiO<sub>3</sub>-H<sub>2</sub>O system, experiments were carried out from 1050 °C to 1650 °C, with starting mixtures containing up to 15.2 wt% H<sub>2</sub>O (Table 2, Fig. 4). All run products contained enstatite and melt or melt only, indicating that melting occurred congruently over the entire temperature range. In one experiment (V704, Table 2) a tiny crystal of forsterite was found as an inclusion in a large enstatite crystal, but this was most likely a consequence of chemical inhomogeneity in the starting mixture. The enstatite liquidus is bracketed at 1650 °C at ~10 wt% H<sub>2</sub>O and at 1500 °C at ~15 wt% H<sub>2</sub>O.

### **3.2 Experimental results at 13 GPa**

Experimental conditions and phase assemblages observed at 13 GPa for both systems Mg<sub>2</sub>SiO<sub>4</sub>-H<sub>2</sub>O and MgSiO<sub>3</sub>-H<sub>2</sub>O are summarized in Table 3. Experiments were performed between 1300 and 1900 °C. In the Mg<sub>2</sub>SiO<sub>4</sub>-H<sub>2</sub>O system, forsterite was found to melt incongruently to an assemblage containing enstatite, forsterite and hydrous melt at temperatures below 1600 °C (Fig. 5). However, the congruent forsterite liquidus could be bracketed at 1700 °C between 13.8 and 20.4 wt% H<sub>2</sub>O and at 1900 °C between 5 and 13.8 wt % H<sub>2</sub>O (Table 3). At 1300 °C, for example, the formation of forsterite in equilibrium with melt was observed at the highest bulk water contents (20.4 wt%), while enstatite was

also crystallized at lower bulk H<sub>2</sub>O contents. This is possibly due to the fact that the univariant Fo + En = Liquid curve has moved closer to the Fo-H<sub>2</sub>O join and small variations within the bulk composition causes enstatite to crystallize (Fig. 3). At 1500 °C, the Mg<sub>2</sub>SiO<sub>4</sub> plus 5 wt% H<sub>2</sub>O starting mixture produced forsterite and melt along with minute crystals of MgO (estimated to be <1 vol%). The lower temperature of this experiment compared to others where MgO was not observed implies that the MgO crystals most likely formed due to a slight inhomogeneity in the starting mixture, rather than an incongruent melting reaction. As we do not observe the presence of MgO in any other of the experiments it is likely that the Fo + Per = Liquid univariant curve crosses the Fo-H<sub>2</sub>O join at lower H<sub>2</sub>O contents than studied (Fig 3), which can be then roughly constrained using the study of Presnall and Walter (1993).

In the system MgSiO<sub>3</sub>-H<sub>2</sub>O, enstatite melted congruently at 1900 °C and the liquidus curve was bracketed at this temperature between 4.3 and 10 wt% H<sub>2</sub>O (Fig. 6). However, in some of the experiments performed between 1300 and 1700 °C, the formation of small crystals of stishovite occurred along with enstatite and melt, in agreement with observations of Yamada et al. (2004) at 13.5 GPa. The presence of stishovite may be due to the fact that En + St + L univariant curve has moved near to the En-H<sub>2</sub>O join, or even crossed it (Fig. 3). This phase, however, was observed only as a minor component, ~2 vol %, and is, therefore, not expected to cause significant departures from the determined phase relations. Additionally, the enstatite liquidus curve was bracketed at 1700 °C between 6.2 and 11.8 wt% H<sub>2</sub>O. At 1600 °C, the most H<sub>2</sub>O-rich charge (15.2 wt% H<sub>2</sub>O)

produced an assemblage of enstatite plus melt, which constrains the minimum H<sub>2</sub>O concentration of the liquidus melt at this temperature.

## 4. Discussion

### 4.1 Model for hydrous melting of Mg<sub>2</sub>SiO<sub>4</sub> and MgSiO<sub>3</sub>

A number of studies have examined the melting point depression of silicate minerals as a function of H<sub>2</sub>O content in the melt using the cryoscopic equation (e.g. Silver and Stolper 1985; Medard and Grove, 2008; Hirschmann et al., 2009; Myhill et al., 2016). For Mg<sub>2</sub>SiO<sub>4</sub> at the liquidus, for example,

$$\ln a_{\text{Mg}_2\text{SiO}_4}^{\text{melt}} = \frac{-\Delta_m G^\circ}{RT} \quad (1)$$

where  $\Delta_m G^\circ$  is the standard state Gibbs free energy of melting of pure forsterite (see Appendix) and  $a_{\text{Mg}_2\text{SiO}_4}^{\text{melt}}$  is the activity of the Mg<sub>2</sub>SiO<sub>4</sub> component in the binary Mg<sub>2</sub>SiO<sub>4</sub>-H<sub>2</sub>O melt. At temperatures below the pure forsterite melting point,  $\Delta_m G^\circ$  can be determined by integrating the entropy of melting of pure Mg<sub>2</sub>SiO<sub>4</sub>,  $\Delta_m S^\circ$ , between the temperature of interest,  $T$ , and the anhydrous melting point,  $T_m$ . Assuming that  $\Delta_m S^\circ$  is constant with temperature, Eq. (1) becomes:

$$\ln a_{\text{Mg}_2\text{SiO}_4}^{\text{melt}} = \frac{\Delta_m S^\circ (T - T_m)}{RT} \quad (2)$$



330

331 The standard entropies of melting for  $\text{Mg}_2\text{SiO}_4$  and  $\text{MgSiO}_3$  solid phases have been  
332 derived from calorimetric measurements at 1 bar (e.g. Navrotsky et al. 1989; Richet et al.,  
333 1993) and expressions for  $\Delta_m S^\circ$  at higher pressures can be determined from data on the  
334 anhydrous melting curves combined with equations of state for solid and liquid  $\text{Mg}_2\text{SiO}_4$   
335 or  $\text{MgSiO}_3$  (see Appendix).

336

337 Use of the cryoscopic equation requires a plausible relationship between the activity and  
338 concentration of silicate species in the hydrous melt, which will depend on the  $\text{H}_2\text{O}$   
339 concentration in the melt and its dissolution mechanism. Empirical molecular mixing of  
340  $\text{Mg}_2\text{SiO}_4$  or  $\text{MgSiO}_3$  and  $\text{H}_2\text{O}$  does not produce a sufficient depression of the liquidus to  
341 explain the experimental data and it has long been recognized that upon dissolution in  
342 silicate melts  $\text{H}_2\text{O}$  dissociates into hydroxyl groups bonded to the silicate framework  
343 (Burnham 1975, 1979, 1994; Stolper, 1982; Silver and Stolper, 1989; Zotov and Keppler,  
344 1998), i.e.

345



347

348 Spectroscopic analyses indicate that both molecular  $\text{H}_2\text{O}$  and  $\text{OH}^-$  groups are present in  
349 silicate melts (e.g. Stolper, 1982, Dixon and Stolper, 1995), and their properties are  
350 temperature-dependent (Nowak and Behrens, 1995; Zotov and Keppler, 1998). Silver and  
351 Stolper (1985) proposed a thermodynamic model to describe the effects of  $\text{H}_2\text{O}$   
352 speciation on the activity of silicate melt components. They assumed that all three species

(H<sub>2</sub>O, O<sup>2-</sup> and OH<sup>-</sup>) mix ideally following a homogeneous melt equilibrium (Eq. 3). The activity of the silicate component,  $a_{\text{Mg}_2\text{SiO}_4}^{\text{melt}}$ , is related to the mole fraction of non-protonated oxygen atoms in the melt,  $X_{\text{O}^{2-}}^{\text{melt}}$ , through the expression

$$a_{\text{Mg}_2\text{SiO}_4}^{\text{melt}} = (X_{\text{O}^{2-}}^{\text{melt}})^r \quad (4)$$

where  $r$  is the number of oxygen atoms available for protonation and mixing per formula unit of silicate, with the chosen formula unit being consistent with the value of  $\Delta_m S^\circ$ . Setting  $r=4$  for Mg<sub>2</sub>SiO<sub>4</sub> or 3 for MgSiO<sub>3</sub> implies that H can bond to any of the oxygen atoms in the silicate melt structure.

The extent of H<sub>2</sub>O dissociation in the silicate melt (Eq. 3) is described by the equilibrium constant  $K$ ,

$$K = \frac{(X_{\text{OH}^-}^{\text{melt}})^2}{X_{\text{H}_2\text{O}}^{\text{melt}} X_{\text{O}^{2-}}^{\text{melt}}}$$

(5)

Following mass balance,

$$X_{\text{H}_2\text{O}}^{\text{melt}} = X_{\text{H}_2\text{O}}^{\text{melt}} + 0.5 X_{\text{OH}^-}^{\text{melt}} \quad (6)$$

374 where  $X_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}}$  is the total mole fraction of H<sub>2</sub>O in the silicate-H<sub>2</sub>O melt. Solving Eqs. (5)

375 and (6) simultaneously, subject to the closure constraint

376

$$377 \quad X_{\text{H}_2\text{O}}^{\text{melt}} + X_{\text{OH}^-}^{\text{melt}} + X_{\text{O}^{2-}}^{\text{melt}} = 1 \quad (7)$$

378

379 yields mole fractions of all three species in the hydrous melt. Substituting Eq. (5) and (6)

380 into Eq. (7) yields

381

$$382 \quad X_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}} = 1 - X_{\text{O}^{2-}}^{\text{melt}} + \frac{KX_{\text{O}^{2-}}^{\text{melt}} - \sqrt{(KX_{\text{O}^{2-}}^{\text{melt}})^2 + 4KX_{\text{O}^{2-}}^{\text{melt}} - 4K(X_{\text{O}^{2-}}^{\text{melt}})^2}}{4} \quad (8)$$

383

384 which is evaluated for the fraction of non-protonated oxygen atoms in the melt. The

385 corresponding activity of the silicate melt component is calculated from Eq. (4) and the

386 liquidus temperature is then defined by Eq. (2). In order to compare the results of the

387 model with experimental data,  $X_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}}$  can be converted to  $w_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}}$ , the mass fraction of

388 H<sub>2</sub>O dissolved in the melt using,

389

$$390 \quad w_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}} = \frac{X_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}} M_{\text{H}_2\text{O}}}{X_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}} M_{\text{H}_2\text{O}} + (1 - X_{\text{H}_2\text{O}^{\text{tot}}}^{\text{melt}}) \frac{M_{\text{sil}}}{r}}$$

391 (9)

392

where  $M_{\text{H}_2\text{O}}$  is the molar mass of water (18.015 g/mol) and  $M_{\text{sil}}$  is the molar mass of the silicate formula unit.

#### 4.1.1 Liquidus depression at 6 GPa

Fig. 2 shows the experimental results for the forsterite liquidus as a function of melt  $\text{H}_2\text{O}$  content at 6 GPa compared to liquidus calculations using several limiting cases of the thermodynamic model. The thermodynamic data used to determine the anhydrous melting point of  $\text{Mg}_2\text{SiO}_4$  and  $\Delta_m S^\circ$  at the pressure and temperature of interest are listed in Table A (see Appendix and Supplementary Material).

Three different curves for the  $\text{Mg}_2\text{SiO}_4$  liquidus are shown calculated for different values of the dissociation equilibrium constant,  $K$ . If all  $\text{H}_2\text{O}$  is completely dissociated to  $\text{OH}^-$  ( $K = \infty$ ), the experimental data at the lowest temperatures are in poor agreement with the model as the experimental liquidus becomes less depressed at high  $\text{H}_2\text{O}$  contents. On the other hand, if all  $\text{H}_2\text{O}$  is dissolved in the molecular form ( $K = 0$ ), the predicted liquidus curve is not in agreement with experimental data at any  $\text{H}_2\text{O}$  concentration. The change in slope of the experimental liquidus implies that  $K$  is not constant over the range of experimental temperatures, but must change from a high or infinite value ( $>50$ ) above 1400 °C to  $<10$  below 1300 °C, i.e. molecular  $\text{H}_2\text{O}$  becomes more important as the  $\text{H}_2\text{O}$  saturated solidus is approached. Variations in  $K$  with temperature can be described using the function,

$$\ln K = \frac{a}{T} + b, \quad (10)$$

416

417 which mimics the enthalpic and entropic contributions to  $K$ . The experimental data do not  
418 provide sufficient constraints to determine the  $a$  and  $b$  coefficients in Eq. (10) uniquely  
419 due to their high correlation. Values of  $a \sim -7000$  K and  $b \sim 5.6$  are in reasonable  
420 agreement, however, with the data and their uncertainties. A different set,  $a = -8000$  K  
421 and  $b = 8$ , recently proposed for alkaline basalt by Lesne et al. (2011) based on  
422 spectroscopic measurements would also just fit the experimental uncertainties, but start to  
423 diverge at temperatures below 1300 °C. The experimental data can only be used to imply  
424 a qualitative, strong dependence of  $K$  on temperature. Independent *in-situ* spectroscopic  
425 data would be required to provide a more accurate estimate of this dependence.

426

427 Although the model is relatively simple, improvements that would provide a significantly  
428 better fit to the experimental data are relatively limited, without making the model  
429 completely empirical. For example, a slightly better agreement between the liquidus  
430 curve and the experimental data at ~1450 °C can only be achieved by decreasing the  
431 standard entropy of forsterite melting at 1 bar, which is already near the lower limit  
432 derived from calorimetric studies (see Appendix). Non-ideal mixing can be included in  
433 the model, however, a simple symmetric mixing parameter between the  $\text{Mg}_2\text{SiO}_4$  and  
434  $\text{H}_2\text{O}$  components produces no significant improvement of the fit. In addition, such terms  
435 have been shown to be unnecessary to describe the effect of  $\text{H}_2\text{O}$  on melting at lower  
436 temperatures, where non-ideal effects should be even more important (Silver and Stolper,  
437 1985).

438

We further compare our experimental results with the model of Tenner et al. (2012a), which is based on the limiting case where all H<sub>2</sub>O dissolves as OH<sup>-</sup>. In Fig. 2, the liquidus is calculated according to this model using the same thermodynamic data as above and assuming  $r = 4$  (random protonation of all oxygen atoms), which is analogous to using a single-oxygen formula unit for the silicate end-member (Tenner et al. 2012a; their Eqs. 9 and 11). The predicted liquidus is substantially different from that obtained from the Silver and Stolper (1985) model with  $K = \infty$ , although both models should be equivalent in describing the liquidus depression when H<sub>2</sub>O dissolves completely as OH<sup>-</sup>. The difference arises in the conversion relationships for the mass fraction of H<sub>2</sub>O by Silver and Stolper (1985) and Tenner et al. (2012a). To bring these two models to numerical consistency, the following relationship would have to be used to calculate the mole fraction of OH<sup>-</sup> in the melt from the H<sub>2</sub>O mass fraction,

$$X_{OH^-}^{melt} = 2 \frac{w_{H_2O^{tot}}^{melt} / M_{H_2O}}{w_{H_2O^{tot}}^{melt} / M_{H_2O} + (100 - w_{H_2O^{tot}}^{melt}) / M_{sil}}, \quad (11)$$

rather than the conversion equation proposed by Tenner et al. (2012a). The model of Tenner et al. (2012a) has been found to quite accurately reproduce the liquidus of experiments performed in natural complex systems when silicates are mixed on a 3-oxygen formula basis. However, the model does not reproduce data on Mg<sub>2</sub>SiO<sub>4</sub> at 6 GPa, regardless of the silicate molecular unit considered, providing an independent confirmation that H<sub>2</sub>O upon dissolution in silicate melt incompletely dissociates to OH<sup>-</sup>.

A further complexity in the model would be to consider the possibility that not all of the oxygen atoms in the melt structure are available for protonation but, for example,  $r = 1$  or 2 per 4-oxygen formula unit (silicate polyhedron) due to local avoidance or ordering principles. This consideration raises two issues, however. First, it would imply a maximum limit for  $\text{H}_2\text{O}$  solubility in the melt, which appears to be not the case. Second, if the number of oxygen sites, which are accessible for proton bonding became an adjustable parameter and were allowed to change, for example, with the  $\text{H}_2\text{O}$  concentration, the resulting fit parameters would be highly correlated with  $K$ . These parameters cannot be meaningfully constrained without an independent estimate of  $K$ . Therefore, the Silver and Stolper (1985) model with temperature-dependent speciation in the melt supported by current estimates for  $\Delta_m S^\circ$  of forsterite and the pressure-temperature melting curve of anhydrous forsterite appears to provide an adequate and well-constrained approximation of the experimental data.

In Fig. 4 experimental results bracketing the  $\text{MgSiO}_3\text{-H}_2\text{O}$  liquidus at 6 GPa are compared with the same set of models as described above. The model that considers complete dissociation to  $\text{OH}^-$  ( $K = \infty$ ) agrees with experimental data at the highest temperatures investigated (above 1600 °C). At lower temperatures, the experimental data again imply a shallower liquidus slope that is not consistent with the complete dissociation of  $\text{H}_2\text{O}$  into  $\text{OH}^-$ . On the other hand, mixing with molecular  $\text{H}_2\text{O}$  only ( $K = 0$ ) results in a liquidus curve far outside of the experimental uncertainties. A model that considers variation of  $K$  with temperature (Eq. 10) fulfils the constraints imposed by the experiments, although a large range of parameters in this equation can provide an

adequate fit to the data. The curve in Fig. 4 was calculated with values of  $a = -6000$  K and  $b = 4.5$  with  $K$  decreasing from  $\sim 7$  at  $2100^\circ\text{C}$  to  $\sim 2$  at  $1300^\circ\text{C}$ . In addition, two models from Tenner et al. (2012a) that assume mixing of silicate molecules with 1- and 3-oxygen formula units, respectively, are shown in Fig. 4. The model of Tenner et al. (2012a) based on 1-oxygen per formula unit predicts values within the experimental uncertainties. However, these authors find the best agreement with melting data using natural peridotite composition when a 3-oxygen silicate molecule is assumed but, as shown in Fig. 4, this is in poor agreement with the data in this simple  $\text{MgSiO}_3\text{-H}_2\text{O}$  subsystem.

Both enstatite and forsterite melting experiments at 6 GPa can be described by Silver and Stolper (1985) models that assume mixing of H on all silicate oxygen atoms and a temperature-dependent dissociation of  $\text{H}_2\text{O}$ , which proceeds towards complete  $\text{OH}^-$  formation above  $\sim 1400^\circ\text{C}$ . It is interesting to note that the mass fraction (wt %) of  $\text{H}_2\text{O}$  in the liquidus melt at a given temperature is nearly identical at 6 GPa for both  $\text{MgSiO}_3$  and  $\text{Mg}_2\text{SiO}_4$  over the entire temperature range.

#### **4.1.2 Liquidus depression at 13 GPa**

In Fig. 5 experiments bracketing the  $\text{Mg}_2\text{SiO}_4\text{-H}_2\text{O}$  liquidus at 13 GPa are shown and compared to the same models as described for the results at 6 GPa. The melting of pure  $\text{Mg}_2\text{SiO}_4$  becomes incongruent above 10 GPa, with  $\text{Mg}_2\text{SiO}_4$  reacting to produce  $\text{MgO}$  and melt at the solidus (Presnall and Walter, 1993). Upon the addition of  $\text{H}_2\text{O}$  to the system, melting becomes congruent between  $1700\text{-}1900^\circ\text{C}$  (Table 3). For the purpose of



modelling the forsterite liquidus, thermodynamic data for congruent  $\text{Mg}_2\text{SiO}_4$  melting at lower pressures have been extrapolated using the melt model of de Koker and Stixrude (2009) to 13 GPa. Models using complete dissociation into  $\text{OH}^-$  by Silver and Stolper (1985) with  $K = \infty$  and by Tenner et al. (2012a) do not reproduce the experimental data (Fig. 5). The best agreement with the experimental liquidus is found for the limiting case of no dissociation, that is, mixing of molecular  $\text{H}_2\text{O}$  ( $K = 0$  or 0.2). There are, however, larger inherent uncertainties in performing this evaluation at 13 GPa arising from the melting temperature assumed for anhydrous  $\text{Mg}_2\text{SiO}_4$ . Although the thermodynamic model of de Koker and Stixrude (2009) used here provides some theoretical justification for the extrapolation, the resulting dramatic change predicted in the  $\text{H}_2\text{O}$  speciation most probably arises from resulting inaccuracies in the temperature of metastable forsterite melting. By assuming an anhydrous melting temperature that is 250 °C higher than predicted by the anhydrous melting model, the temperature-dependent model for  $K$  calibrated at 6 GPa for  $\text{Mg}_2\text{SiO}_4$  can be equally applied at 13 GPa. We conclude, therefore, that it is more likely that the anhydrous melting temperature is in error, than that there is a dramatic shift in  $\text{H}_2\text{O}$  speciation at high pressure. This highlights the problems of examining melting point depression in incongruent systems, which are likely to be even more complex for natural multicomponent systems such as mantle peridotite melts.

For  $\text{MgSiO}_3$ , the liquidus depression at 13 GPa is consistent with the Silver and Stolper (1985) model for nearly complete dissociation to  $\text{OH}^-$  in the melt (Fig. 6). While this is in contrast to  $\text{Mg}_2\text{SiO}_4$  at the same pressure, it is in better agreement with the experimental

results at 6 GPa. Introducing a temperature dependence to  $K$  is not justified by the data, within the experimental uncertainties. A molecular  $\text{H}_2\text{O}$  model is far outside of the experimental constraints, however, as is the model of Tenner et al. (2012a).

## **4.2 The effect of pressure on liquidus depression due to $\text{H}_2\text{O}$ in simple and complex silicate systems**

The liquidus depression under hydrous conditions in comparison to the anhydrous melting point is shown for both the  $\text{MgSiO}_3\text{-H}_2\text{O}$  and  $\text{Mg}_2\text{SiO}_4\text{-H}_2\text{O}$  systems at 6 and 13 GPa in Fig. 7. Experimental data of Kushiro et al. (1968) for  $\text{MgSiO}_3\text{-H}_2\text{O}$  at 1 GPa and between 1375 and 1525 °C are used in order to provide an additional comparison; a value of  $K = 0.5$  in the Silver and Stolper (1985) formulation provides a good fit to these data. For  $\text{MgSiO}_3$ , pressure enhances the influence of  $\text{H}_2\text{O}$  in depressing the melting temperature in line with thermodynamic estimates for the entropy of fusion and the anhydrous melting curve of  $\text{MgSiO}_3$ . The effect of pressure on the water-driven melting point depression of  $\text{MgSiO}_3$  is best explained by an increase in the dissociation of  $\text{H}_2\text{O}$  with increasing pressure, with essentially no molecular  $\text{H}_2\text{O}$  being involved above 1400 °C, at pressures of 6 GPa and higher.

For the  $\text{Mg}_2\text{SiO}_4\text{-H}_2\text{O}$  binary, however, there is an apparent decrease in the effect of  $\text{H}_2\text{O}$  on liquidus depression between 6 and 13 GPa. As discussed above this is most likely caused by an underestimate in the metastable melting temperature of anhydrous  $\text{Mg}_2\text{SiO}_4$ , which melts incongruently above 10 GPa. If the anhydrous melting temperature is assumed to be 250 °C higher at 13 GPa, then the effect on liquidus depression is reversed.

This implies that the extrapolated melting curve for  $\text{Mg}_2\text{SiO}_4$  is incorrect. The Silver and Stolper (1985) model with values of  $K = \sim 0.2$  at 2100 °C and approaching 0 at 1300 °C successfully reproduce experimental data of Hodges (1974) at 3 GPa in the forsterite- $\text{H}_2\text{O}$  system. Data at 3 GPa show lower melting temperature depression in comparison to those at 6 GPa, is in agreement with the pressure trend observed in the enstatite- $\text{H}_2\text{O}$  system and further suggesting a positive effect of pressure on melting temperature depression.

In Fig. 7, data for the liquidus depression due to  $\text{H}_2\text{O}$  for melts of natural peridotite composition are shown from Tenner et al. (2012a) at 3.5 GPa and Novella and Frost (2014) at 6 GPa. The depression of melting due to  $\text{H}_2\text{O}$  is much smaller for these complex melts compared to either of the simple systems at the same pressure. This difference is partly due the lower anhydrous liquidus temperatures of the natural multicomponent melts. As indicated by Eq. (2) the magnitude of the liquidus depression should increase with the anhydrous melting temperature, as observed in all experiments. In Fig. 7 these data are fitted using a Silver and Stolper (1985) model with molar mass of 37 g/mol per single-oxygen formula unit and a  $\Delta_m S^\circ = 0.4 \text{ J}/(\text{K}\cdot\text{g})$  (Tenner et al., 2012a; Kojitani and Akaogi, 1997). A constant value of  $\Delta_m S^\circ$  in Eq. (2) is assumed at all pressures and temperatures and the anhydrous melting temperatures are taken from Walter (1998). The best correspondence with experiments at 3.5 GPa requires a temperature dependent value of  $K$ , which starts near unity close to the anhydrous melting temperature but decreases to effectively zero below 1200 °C. Although there is only one data point available at 6 GPa the depression of melting is consistent with a similar model as at 3.5 GPa, with the only difference being the anhydrous melting temperature. The

Silver and Stolper (1985) model, therefore, implies a much smaller extent of  $\text{H}_2\text{O}$  dissociation into  $\text{OH}^-$  and a greater proportion of molecular  $\text{H}_2\text{O}$  in multicomponent melts when compared to simple systems. This difference may have several origins, however. First, the value of  $\Delta_m S^\circ$  employed for peridotite melt is poorly constrained as it is derived from calorimetric measurements in the  $\text{CaO-MgO-Al}_2\text{O}_3\text{-SiO}_2$  system at 1 bar (Kojitani and Akaogi, 1997) and it may not suitably account for the effects of pressure and composition. Second, it is possible that certain components present in the natural peridotite melt compositions, such as  $\text{Al}_2\text{O}_3$ , cause a reduction in the effect of  $\text{H}_2\text{O}$  on the configurational entropy of the melt. As a result of such distinct behaviour, the effect of  $\text{H}_2\text{O}$  on melting in such simple systems may be quite far away from that in complex mantle melts.

Although the justification as to how the melt  $\text{OH}^-$  mole fraction is calculated is somewhat unclear in the model of Tenner et al. (2012a), particularly in relation to the Silver and Stolper (1985) model, it is interesting to note that it does closely predict the liquidus depression for complex peridotitic melts at both 3.5 and 6 GPa. The model is based on a 3-oxygen melt described by Eq. (11) and it predicts curves identical to those shown in Fig. 7 using the Silver and Stolper (1985) model for the natural peridotite data at 3.5 and 6 GPa. Although only empirical in its nature, it tends to numerically mimic decreasing protonation of the oxygen sites in the silicate melt structure, and it produces a good fit to the natural multicomponent data with fewer adjustable parameters. As there seems to be no clear justification to the way in which the  $\text{OH}^-$  mole fraction is derived in the Tenner et al. (2012a) model, the predictive capacity may be a coincidence.

599

#### 600 **4.2.1 Hydrous melts along adiabatic temperature gradient**

601 A number of seismic observations appear to show evidence for low shear wave velocities  
602 at the base of the upper mantle above the 410 km discontinuity (e.g. Song et al., 2004;  
603 Vinnik et al., 2009; Jusbinken et al., 2010; Tauzin et al., 2010). These observations have  
604 been proposed to result from the presence of low degree volatile-bearing melts at these  
605 depths (Bercovici and Karato, 2003). Assuming that the upper mantle has a constant H<sub>2</sub>O  
606 content, it might be possible to explain the visibility of H<sub>2</sub>O induced melting at the base  
607 of the upper mantle if pressure enhances melt productivity at these conditions. One way  
608 that this might occur is if less H<sub>2</sub>O were required to stabilise melts with increasing  
609 pressure.

610

611 In Fig. 7 the speciation model of Silver and Stolper (1985) using a temperature-dependent  
612 value of  $K$  varying between  $\sim 1$  and 0 at 3.5 and 6 GPa is extrapolated to 13 GPa by  
613 assuming an anhydrous melting temperature of 1900 °C at this pressure (Takahashi,  
614 1986). The model by Tenner et al. (2012a) would predict an identical liquidus depression.  
615 The results of this extrapolation are given in Fig. 8, which shows the H<sub>2</sub>O content in  
616 MgSiO<sub>3</sub>, Mg<sub>2</sub>SiO<sub>4</sub> and peridotite melts determined at upper mantle adiabatic temperatures  
617 (potential temperature  $\sim 1350$  °C).

618

619 With increasing pressure the amount of H<sub>2</sub>O required to stabilize Mg<sub>2</sub>SiO<sub>4</sub> melt along a  
620 mantle adiabat increases quite substantially between 6 and 13 GPa. This means that for a  
621 system with a fixed H<sub>2</sub>O content, the percentage of melt will decrease towards conditions

of the base of an upper mantle. This effect would work in conjunction with an increase in the forsterite-melt H<sub>2</sub>O partition coefficient with pressure (see Hirschmann et al., 2009; Novella et al., 2014), which would also act to decrease the percentage of melting for a given bulk H<sub>2</sub>O concentration. By contrast, the H<sub>2</sub>O content of a MgSiO<sub>3</sub> melt appears to actually decrease slightly between 6 and 13 GPa, which could in theory lead to an increase in the percentage of melting for a fixed H<sub>2</sub>O content. However, the decrease in melt H<sub>2</sub>O content is small and this effect would be counteracted by an increase in the enstatite-melt partitioning coefficient with pressure, calculated from the literature (Rauch and Keppler, 2002; Yamada et al., 2004; Withers and Hirschmann, 2007; Withers et al., 2011) and melt H<sub>2</sub>O content from this study. Peridotite melts are also predicted to require more H<sub>2</sub>O to be stable at higher pressures, although the H<sub>2</sub>O concentrations tend to vary very little towards the base of the upper mantle similar in fact to MgSiO<sub>3</sub>. This analysis indicates that there is no evidence for increasing melt productivity due to H<sub>2</sub>O towards the base of the Earth's upper mantle, although it has to be recognised that there is some uncertainty as the results for peridotite are being extrapolated above 6 GPa.

In order for the proportion of hydrous melting to increase and therefore be seismically more visible towards the base of the upper mantle, the bulk mantle at these conditions would need to be significantly enriched in H<sub>2</sub>O. Such a localized enrichment in H<sub>2</sub>O at this depth would require an effective fractionation process to maintain high H<sub>2</sub>O concentrations at this depth. Bercovici and Karato (2003) proposed that hydrous melts formed under these conditions may be neutrally buoyant and, therefore, separate from the upwelling mantle and concentrate to form a low-velocity zone. Such a separation will

depend on melt density, which in turn will depend on the melt H<sub>2</sub>O concentration. Melt density experiments by Matsukage et al. (2005) favour such a scenario, although their H<sub>2</sub>O concentrations (~6 wt%) are approximately 50 % of those estimated in this study for natural peridotitic melts at the bottom of the upper mantle (Fig. 8). Following the density systematics of Jing and Karato (2009), partial melts in equilibrium with peridotite at 13 GPa should be much less dense than the surrounding mantle if the H<sub>2</sub>O contents in the melt are close to those predicted here (Fig. 8).

## Acknowledgements

Hubert Schulze, Raphael Njul, Stephan Übelhack, Heinz Fischer, Detlef Krausse and Sven Linhardt are kindly acknowledged for their technical support. The present study was supported by the Elitenetzwerk Bayern international graduate school “Structure, Reactivity and Properties of Oxide Materials”. D.N. further acknowledges funding from the French Government Laboratory of Excellence initiative n°ANR-10-LABX-0006, the Région Auvergne and the European Regional Development Fund. This is Laboratory of Excellence ClerVolc contribution number xx. D.D. would like to acknowledge personal support by the Czech Science Foundation Project Nr. 210/12/0986. We thank associate editor Mike Toplis and Mike Walter and an anonymous reviewer for comments that significantly improved the manuscript.

## Appendix: Thermodynamic relations and parameters

The Mie-Grüneisen equations of state (EOS) were employed to determine the Gibbs energy of melting ( $\Delta_m G^0$ ) of forsterite and enstatite required for the cryoscopic equation

in the  $\text{Mg}_2\text{SiO}_4\text{-H}_2\text{O}$  and  $\text{MgSiO}_3\text{-H}_2\text{O}$  binaries. Expressions to define the Gibbs energy for  $\text{Mg}_2\text{SiO}_4$  and  $\text{MgSiO}_3$  were taken from Stixrude and Lithgow-Bertelloni (2011) for solids and from de Koker and Stixrude (2009) for liquids and are based on the fundamental thermodynamic relation between the Helmholtz energy ( $F$ ) and the Gibbs energy:

$$G(P, T) = F(V, T) + PV, \quad (\text{A.1})$$

where  $V$  is the volume,  $P$  is the pressure and  $T$  is the temperature. The Helmholtz energy at elevated pressure and temperature is obtained by stepwise integration from ambient conditions ( $T_0 = 298.15$  K,  $P_0 = 101325$  Pa) *via* isothermal compression at reference temperature (c) and isochoric heating (th), which accounts for the effect of thermal vibrations:

$$F(V, T) = F(P_0, T_0) + \Delta F_c(T_0) + \Delta F_{th}(V). \quad (\text{A.2})$$

The contribution to the Helmholtz energy due to isothermal compression ( $\Delta F_c$ ) was calculated from the third-order Birch-Murnaghan EOS (Murnaghan, 1937; Birch, 1947; e.g. Poirier, 2000):

$$\Delta F_c(T_0) = 9K_0V_0 \left[ \frac{f^2}{2} + \frac{af^3}{3} \right]. \quad (\text{A.3})$$



The EOS is based on the finite strain theory, where the finite strain ( $f$ ) and the factor  $a$  are calculated as follows:

$$f = \frac{1}{2} \left( \frac{V_0}{V} \right)^{2/3} - 1 \quad (\text{A.4})$$

and

$$a = \frac{3}{2} (K'_0 - 4) . \quad (\text{A.5})$$

In this formulation,  $K_0$  and  $V_0$  correspond to the bulk modulus and the volume, respectively, at the reference pressure and temperature, and  $K'_0$  is the first pressure derivative of the bulk modulus at reference conditions. The volume ( $V$ ) of the phase at the pressure and temperature of interest was found in order to satisfy the following relation:

$$P = P_c + P_{th} , \quad (\text{A.6})$$

where

$$P_c = 3K_0 f (2f + 1)^{5/2} (1 + fa) . \quad (\text{A.7})$$

711 The equations of state for thermal pressure ( $P_{th}$ ) and calculation of the relevant  
 712 thermodynamic properties differ for liquid and solid phases. For the liquid phases, the  
 713 thermal pressure is defined by

$$715 \quad P_{th} = \frac{\gamma}{V} c_v (T - T_0) \quad (A.8)$$

716  
 717 where  $c_v$  is the isochoric heat capacity, and  $\gamma$ , representing the Grüneisen parameter, is a  
 718 function of volume as follows

$$720 \quad \gamma = \gamma_0 + \gamma' \left[ \frac{V}{V_0} - 1 \right] \quad (A.9)$$

721  
 722 where  $\gamma_0$  is the Grüneisen parameter at the reference conditions and  $\gamma'$  is its first  
 723 derivative with respect to the volume. The thermal contribution to the Helmholtz energy  
 724 ( $\Delta F_{th}$ ) of a liquid is then defined by:

$$725 \quad \Delta F_{th}(V) = -S_0(T - T_0) - c_v \left[ T \ln \left[ \frac{T}{T_0} \right] - (T - T_0) \right] - c_v (T - T_0) (\gamma_0 - \gamma') \ln \left[ \frac{V}{V_0} \right] + (\gamma - \gamma_0) \quad (A.10)$$

729 where  $S_0$  is the standard entropy of the substance at a reference state chosen to be  
 730 consistent with literature data as described above (see Table A).

731

For the solid phases, a slightly different approach was used starting with the calculation of the volume at the pressure and temperature of interest ( $V$ ). The thermal pressure of the solid phase was determined using an expression for the Debye thermal energy ( $E_{th}$ ), that is,

$$P_{th} = \frac{\gamma}{V} [E_{th}(V, T) - E_{th}(V, T_0)] \quad (A.11)$$

and, in this case, the Grüneisen parameter is calculated as

$$\gamma = \gamma_0 \left( \frac{V}{V_0} \right)^{q_0}, \quad (A.12)$$

where  $q_0$  is a constant, and the thermal internal energy ( $E_{th}$ ) is defined by the Debye model for the lattice vibrational energy

$$E_{th} = 9nRT \left( \frac{T}{\theta} \right)^3 \int_0^{\frac{T}{\theta}} \frac{t^3}{e^t - 1} dt, \quad (A.13)$$

where  $R$  is the universal gas constant,  $n$  is the number of atoms per formula unit,  $t = \theta/T$ , with the Debye temperature ( $\theta$ ) calculated as

$$\theta = \theta_0 e^{\frac{\gamma_0 - \gamma}{q_0}}. \quad (A.14)$$

753

754 The corresponding expression for the thermal Helmholtz energy ( $F_{\text{th}}$ ) of the solid phases,  
755 defined as the Debye approximation of the quasi-harmonic vibrational density of states, is  
756 as follows:

757

758 
$$F_{\text{th}}(V) = 9nRT \left( \frac{T}{\theta} \right)^3 \int_0^{\theta/T} \ln(1 - e^{-t}) t^2 dt . \quad (\text{A.15})$$

759

760 The thermal contribution to the Helmholtz energy ( $\Delta F_{\text{th}}$ ) of the solid phases between the  
761 reference temperature ( $T_0$ ) and that of interest ( $T$ ) at the constant volume of interest ( $V$ ), is  
762 found by difference:

763

764 
$$\Delta F_{\text{th}}(V) = F_{\text{th}}(V, T) - F_{\text{th}}(V, T_0) . \quad (\text{A.16})$$

765

766 The thermodynamic properties employed in the calculations of the Gibbs energy for solid  
767 and liquid  $\text{Mg}_2\text{SiO}_4$  and  $\text{MgSiO}_3$  are summarized in Table A and are based on previous  
768 compilations by de Koker and Stixrude (2009) and Stixrude and Lithgow-Bertelloni  
769 (2011) for liquid and solid phases, respectively. The Helmholtz energy for liquid  
770 substances at reference conditions ( $F_0$ ) was empirically calculated from the room pressure  
771 melting temperatures as explained by Liebske and Frost (2012). The reference state  
772 volumes ( $V_0$ ) and entropies ( $S_0$ ) for the liquid end-members were slightly altered  
773 compared to those reported by de Koker and Stixrude (2009) in order to obtain better  
774 agreement with the experimental melting temperatures and to be consistent with  
775 calorimetric data for the enthalpy of melting of  $\text{MgSiO}_3$  and  $\text{Mg}_2\text{SiO}_4$  (Navrotsky et al.,

1989; Richet et al., 1993). Specifically, the thermodynamic data of  $\text{Mg}_2\text{SiO}_4$  liquid of de Koker and Stixrude (2009) had to be modified such that the value of  $\Delta_m S^\circ$  for forsterite at 1 bar was consistent with 52.7 J/(K·mol) proposed by Navrotsky et al. (1989). This is at the lower end of the range of values reported in the literature, which vary from 70 to 47.5 J/(K·mol) (Bottinga, 1985; Navrotsky et al., 1989; Richet et al., 1993; Tangeman et al., 2001). Values for the standard heat capacity and volume of  $\text{Mg}_2\text{SiO}_4$  liquid were then also adjusted to bring the model into agreement with experimental data on the melting curve of  $\text{Mg}_2\text{SiO}_4$  (Davis and England, 1964; Kato and Kumazawa, 1985; Presnall and Walter, 1993).

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# 967 **Figure captions**

968 **Fig. 1:** Backscattered electron (BSE) images of experiments performed at 6 GPa in the  
 969 Mg<sub>2</sub>SiO<sub>4</sub>-H<sub>2</sub>O system. The bright material is the Pt capsule. Grey crystals (50 to 100 µm  
 970 across) of forsterite can be easily distinguished from the fine grain quenched melt. **(a):**  
 971 figure corresponds to experiment V649 (Table 2) where in order from left to right are  
 972 sample chambers containing starting mixtures of Mg<sub>2</sub>SiO<sub>4</sub> plus 5, 10, 15 and 20.4 wt%  
 973 H<sub>2</sub>O in the bulk. The third chamber from the left shows two quench textures in the same  
 974 charge with different fibrous grain sizes, likely formed due to differences in nucleation  
 975 and crystal growth (see text). **(b):** BSE image of experiment V660 (Table 2) where, from  
 976 left to right, starting mixtures of Mg<sub>2</sub>SiO<sub>4</sub> with 7.9, 9.7, 13.8 and 18.3 wt% H<sub>2</sub>O (bulk)  
 977 were employed.

**Fig. 2:** Phase diagram of the  $\text{Mg}_2\text{SiO}_4\text{-H}_2\text{O}$  system at 6 GPa showing experimental data and models for the liquidus curves (described in the text). Data points determined in this study are displayed by black and grey symbols (Table 2) while data from Luth (1993) at 6 GPa and Inoue (1994) at 5.5 GPa are shown by blue and green symbols, respectively. Data from Luth (1993) and Inoue (1994) were determined for bulk compositions of  $\text{Mg}_2\text{SiO}_4$  plus 20.4 wt%  $\text{H}_2\text{O}$  but are plotted at slightly higher  $\text{H}_2\text{O}$  content to aid visibility. The liquidus at approximately 20 wt%  $\text{H}_2\text{O}$  is  $\sim 200$  °C lower than reported by Inoue et al. (1994) at 5.5 GPa but is in agreement, within uncertainty, with the data of Luth (1993) at 6 GPa. The plotted liquidus curves are all constrained by the dry melting temperature of forsterite at 6 GPa reported by Kato and Kumazawa (1985). Details regarding the different curves are reported in the text. Uncertainties of 1 wt% in the melt composition and 50-100 °C for the temperature of the experiments (see text) are displayed by the error bars.

**Fig. 3:** Indicative ternary phase diagrams in the system  $\text{MgO-SiO}_2\text{-H}_2\text{O}$ . Phase relations are tentatively constrained at 6 (top) and 13 (bottom) GPa by the experimental results reported in this study and the literature. Starting compositions in the forsterite- $\text{H}_2\text{O}$  and enstatite- $\text{H}_2\text{O}$  joins are plotted as black circles, on a molar basis. Fo: forsterite; En: enstatite; Per: periclase; St: stishovite; L: liquid (or melt). The dashed line indicates the  $\text{Fo} + \text{En} = \text{L}$  reaction curve while the dotted lines show the possible location of the  $\text{Fo} + \text{Per} = \text{L}$  (toward MgO corner) and  $\text{En} + \text{St} = \text{L}$  (toward  $\text{SiO}_2$  corner) curves.

**Fig. 4:** The depression of the  $\text{MgSiO}_3$  liquidus curve at 6 GPa as a function of melt  $\text{H}_2\text{O}$  content. Data points determined in this study (Table 2) are displayed by black symbols while green symbols are from Inoue (1994), plotted at slightly higher  $\text{H}_2\text{O}$  content to aid

visibility. Uncertainties of 1 wt% in the melt composition and 50-100 °C for the temperature of the experiments (see text) are displayed by the error bars. Curves describing the liquidus determined by different models as described in the text are also shown. The liquidus curves are all constrained by the dry melting temperature of enstatite at 6 GPa reported by Kato and Kumazawa (1985).

**Fig. 5:** Melting phase relations in the  $\text{Mg}_2\text{SiO}_4\text{-H}_2\text{O}$  system at 13 GPa. Uncertainties of 1 wt% in the melt composition and 50-100 °C for the temperature of the experiments (see text) are displayed. The dry melting temperature of forsterite at 13 GPa was calculated to be 2200 °C by extrapolation of the equations of state of de Koker and Stixrude (2009).

**Fig. 6:** The melting phase relations in the  $\text{MgSiO}_3\text{-H}_2\text{O}$  system at 13 GPa. Uncertainties of 1 wt% in the melt composition and 50-100 °C for the temperature of the experiments (see text) are displayed. The dry melting temperature of enstatite at 13 GPa was calculated to be 2250°C using the model of de Koker and Stixrude (2009). Values of  $a = -8000$  K and  $b = 8$  were employed in the calculation of constant  $K$  (red line).

**Fig. 7:** The depression in the hydrous melting temperature as a function of  $\text{H}_2\text{O}$  for  $\text{MgSiO}_3\text{-H}_2\text{O}$  (black lines),  $\text{Mg}_2\text{SiO}_4\text{-H}_2\text{O}$  (green lines) and natural (blue lines) melt compositions between 1 and 13 GPa. Hydrous garnet peridotite melt compositions are from Tenner et al. (2012a) at 3.5 GPa (red dots) and Novella and Frost (2014) at 6 GPa (grey square). The blue curves are fitted to these data, as described in the text.

**Fig. 8:** Melt  $\text{H}_2\text{O}$  contents as a function of pressure determined at 3.5, 6 and 13 GPa and at temperatures corresponding to a mantle adiabat (1350 °C, 1400 °C and 1500 °C, respectively). Peridotite data are taken from the curves shown in Fig. 7.